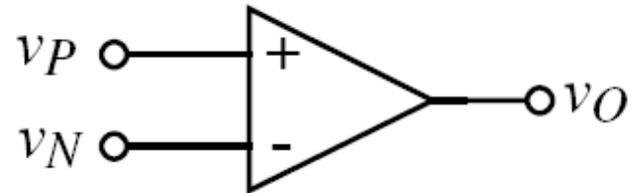


What are Comparators?

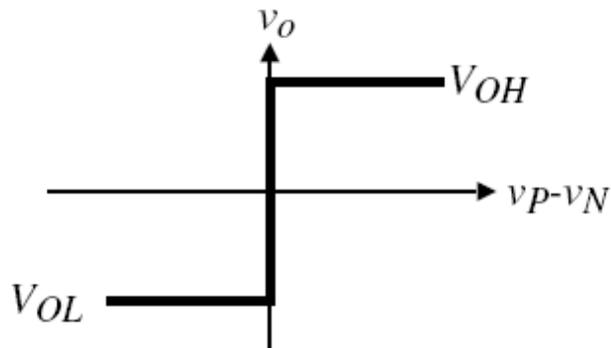
A 1-Bit Analog-Digital Converter

or

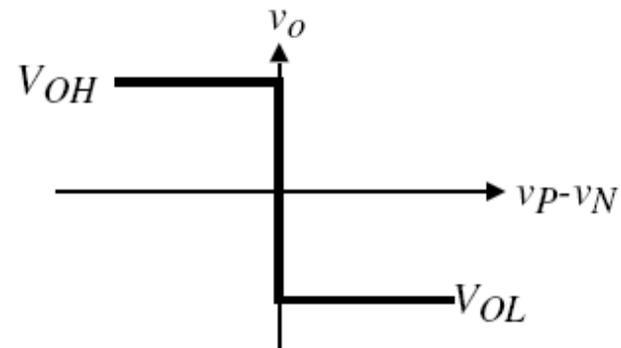
A 1-Bit Quantizer



Inputs Analog Signals and Outputs a Digital Signal



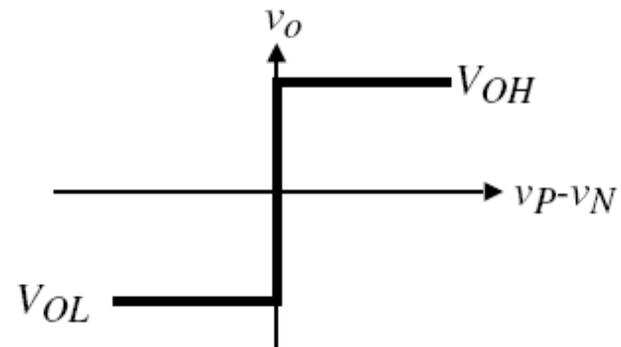
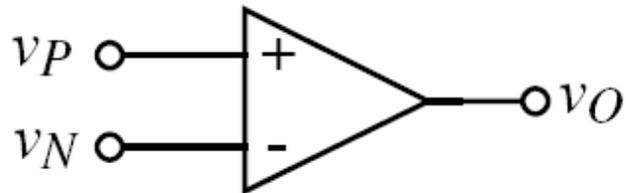
Noninverting Comparator



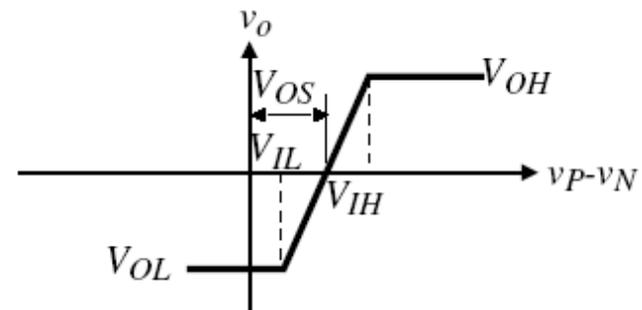
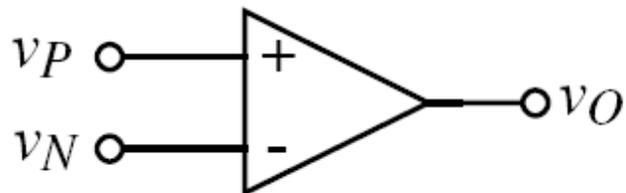
Inverting Comparator

Static Characteristics

Ideal Comparator



Real Comparator



Definitions

V_{OH} = the high output of the comparator

V_{OL} = the low level output of the comparator

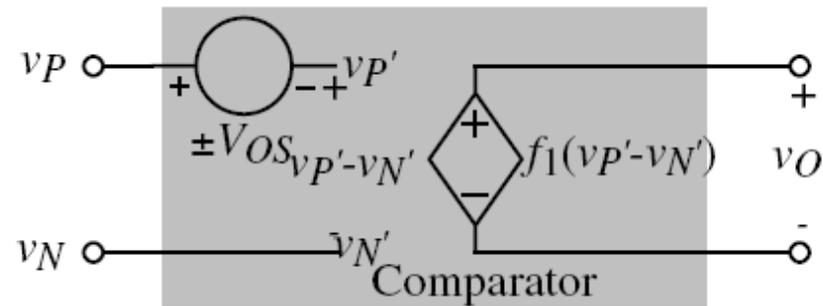
Gain = $A_v = \lim_{\Delta V \rightarrow 0} \frac{V_{OH} - V_{OL}}{\Delta V}$ where ΔV is the input voltage change

V_{IH} = smallest input voltage at which the output voltage is V_{OH}

V_{IL} = largest input voltage at which the output voltage is V_{OL}

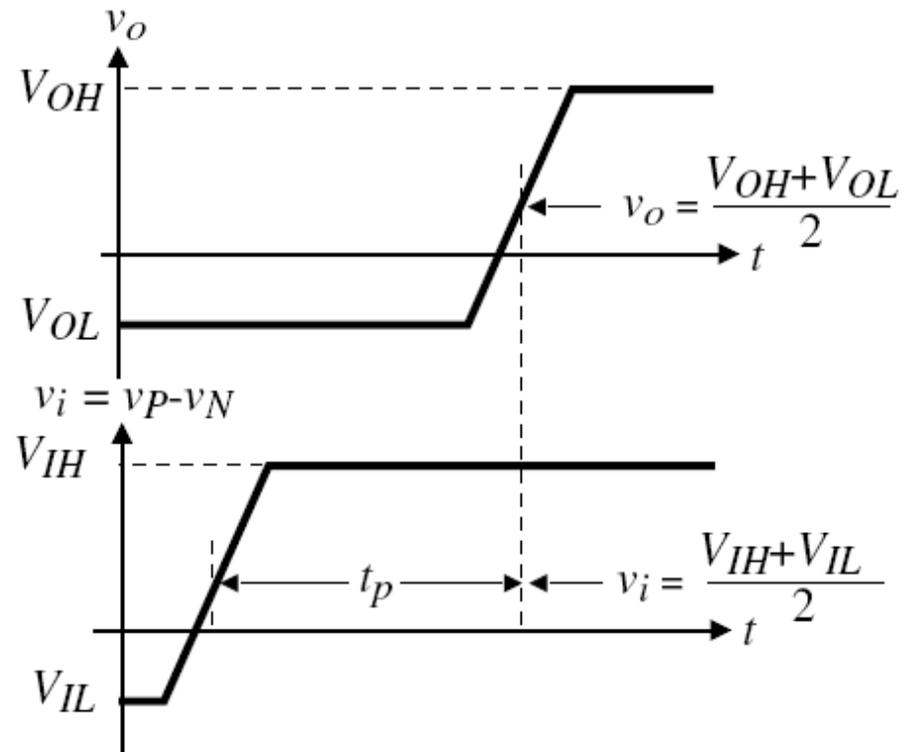
V_{OS} = the input voltage necessary to make the output equal $\frac{V_{OH} + V_{OL}}{2}$ when $v_P = v_N$.

Comparator Macromodel



$$f_1(v_P' - v_N') = \begin{cases} V_{OH} & \text{for } (v_P' - v_N') > V_{IH} \\ A_v(v_P' - v_N') & \text{for } V_{IL} < (v_P' - v_N') < V_{IH} \\ V_{OL} & \text{for } (v_P' - v_N') < V_{IL} \end{cases}$$

Propagation Delay



Propagation Delay = (Rise Time + Fall Time)/2

Propagation Delay

Frequency Domain

$$A_v(s) = \frac{A_v(0)}{\frac{s}{\omega_c} + 1} = \frac{A_v(0)}{s\tau_c + 1}$$

$A_v(0)$ = dc voltage gain of the comparator

$\omega_c = \frac{1}{\tau_c}$ = -3dB frequency of the comparator or the magnitude of the pole

Time Domain

$$v_o(t) = A_v(0) [1 - e^{-t/\tau_c}] V_{in}$$

V_{in} = the magnitude of the step input.

Propagation Delay

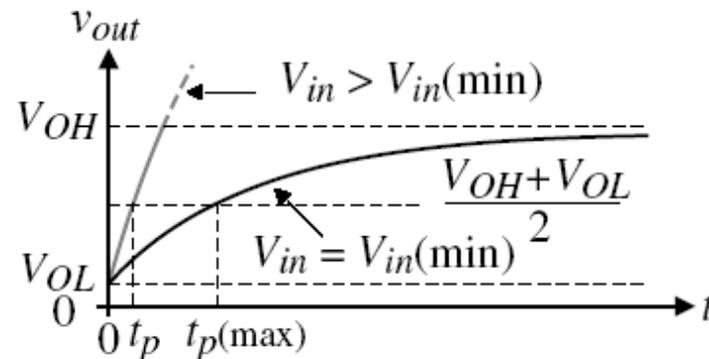
$$\frac{V_{OH}-V_{OL}}{2} = A_v(0) [1 - e^{-t_p/\tau_c}] V_{in} \quad \rightarrow \quad t_p = \tau_c \ln \left[\frac{1}{1 - \frac{V_{OH}-V_{OL}}{2A_v(0)V_{in}}} \right]$$

Define

$$V_{in(\min)} = \frac{V_{OH}-V_{OL}}{A_v(0)} \quad k = \frac{V_{in}}{V_{in(\min)}}$$

Propagation Delay

$$t_p = \tau_c \ln \left[\frac{2k}{2k-1} \right]$$



Slew Rate

For large overdrives, the comparator is limited by Slew Rate

Slew Rate

- **Analysis similar to an operational amplifier**
- **Depends on current charging/discharging a capacitor**

$$\text{Slew Rate} = \frac{dv}{dt} = \frac{I}{C}$$

Propagation Delay when slew rate limited

$$t_p = \Delta T = \frac{\Delta V}{SR} = \frac{V_{OH} - V_{OL}}{2 \cdot SR}$$

Performance Metrics

Maximum Output Voltage

$$V_{OH} = V_{DD} - (V_{DD} - V_{G6(\min)} - |V_{TP}|) \left[1 - \sqrt{1 - \frac{8I_7}{\beta_6(V_{DD} - V_{G6(\min)} - |V_{TP}|)^2}} \right]$$

Minimum Output Voltage

$$V_{OL} = \bar{V}_{SS}$$

Open Loop Gain

$$A_v(0) = \left(\frac{g_{m1}}{g_{ds2} + g_{ds4}} \right) \left(\frac{g_{m6}}{g_{ds6} + g_{ds7}} \right)$$

Frequency Response

$$A_v(s) = \frac{A_v(0)}{\left(\frac{s}{p_1} - 1 \right) \left(\frac{s}{p_2} - 1 \right)} \quad p_1 = \frac{-(g_{ds2} + g_{ds4})}{C_I} \quad p_2 = \frac{-(g_{ds6} + g_{ds7})}{C_{II}}$$

Performance Metrics

Propagation Delay

$$v_{out}(t) = A_v(0)V_{in} \left[1 + \frac{p_2 e^{tp_1}}{p_1 - p_2} - \frac{p_1 e^{tp_2}}{p_1 - p_2} \right]$$

Simplifying

$$v_{out}(t_n) = A_v(0)V_{in} \left[1 - \frac{m}{m-1} e^{-t_n} + \frac{1}{m-1} e^{-mt_n} \right]$$

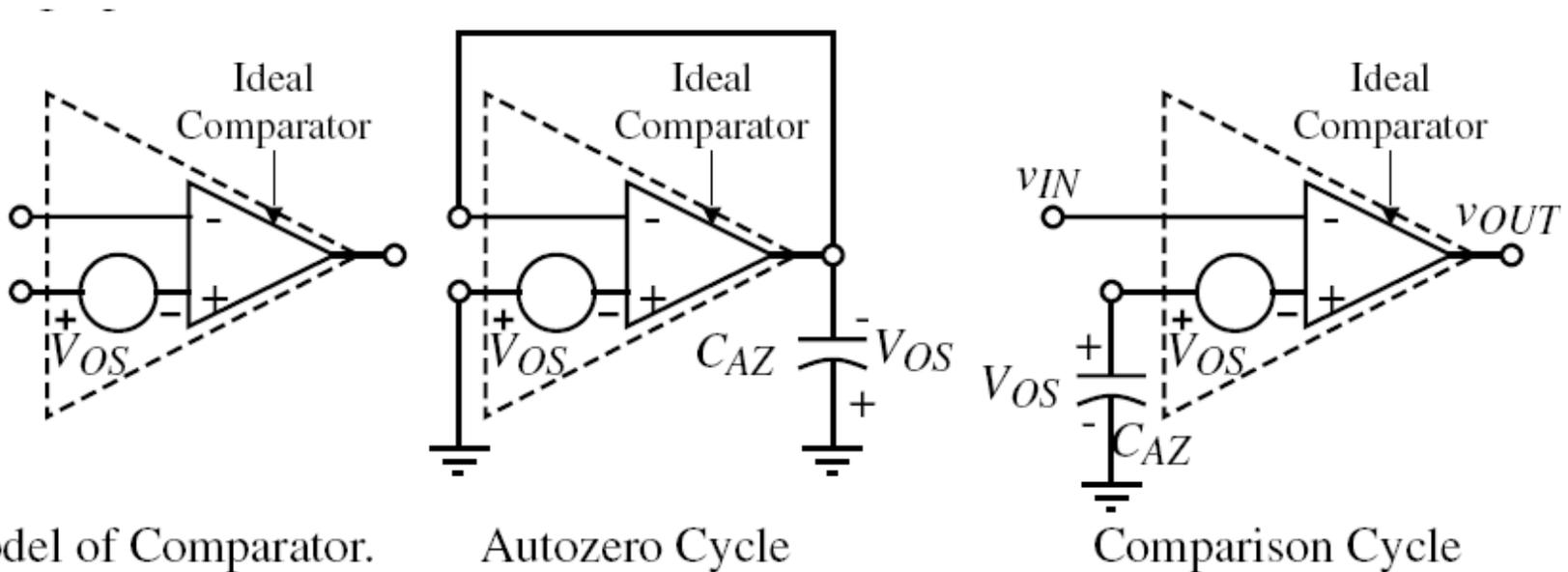
$$m = \frac{p_2}{p_1} \neq 1 \quad \text{and} \quad t_n = -tp_1$$

$$t_{pn} \approx \sqrt{\frac{V_{OH} + V_{OL}}{mA_v(0)V_{in}}} = \sqrt{\frac{V_{in}(\min)}{mV_{in}}} = \frac{1}{\sqrt{mk}}$$

Linear Analysis

Comparator slews if a large input overdrive is applied

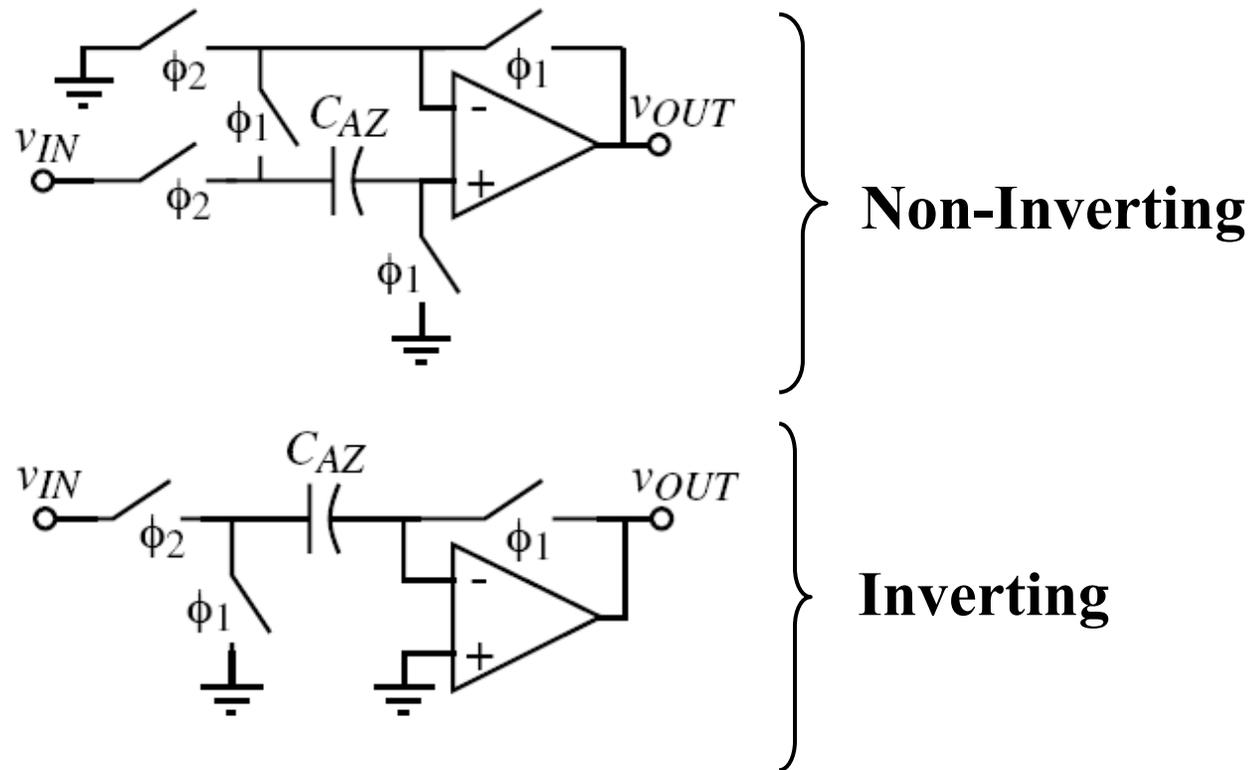
Autozeroing



Key Issues

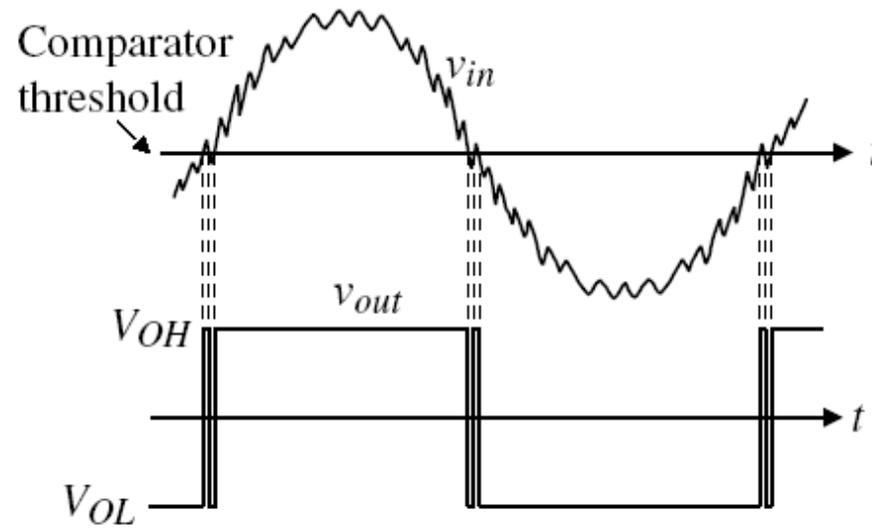
- **Stability during the autozero cycle**
- **Charge Injection during switching**

Autozeroing



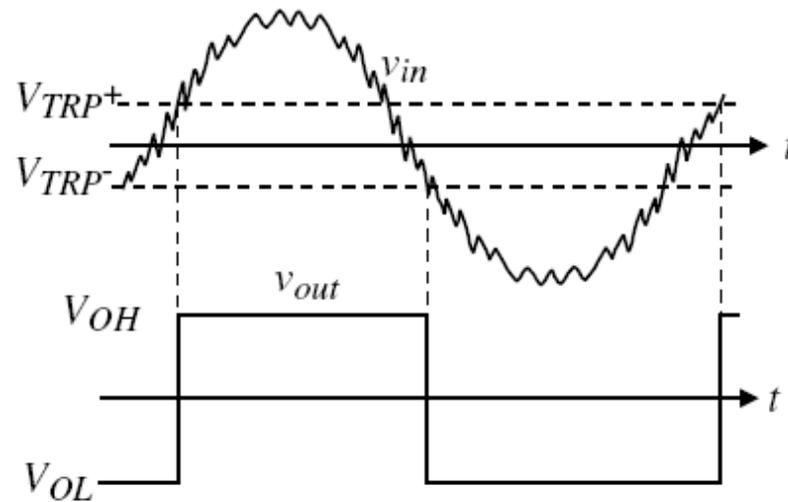
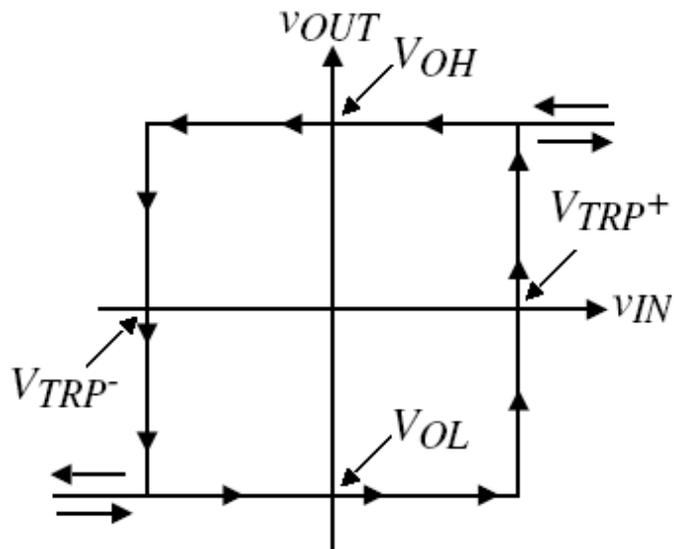
Note: Clocks need to be non-overlapping

Influence of Noise



Noise can result in false switching in the comparator

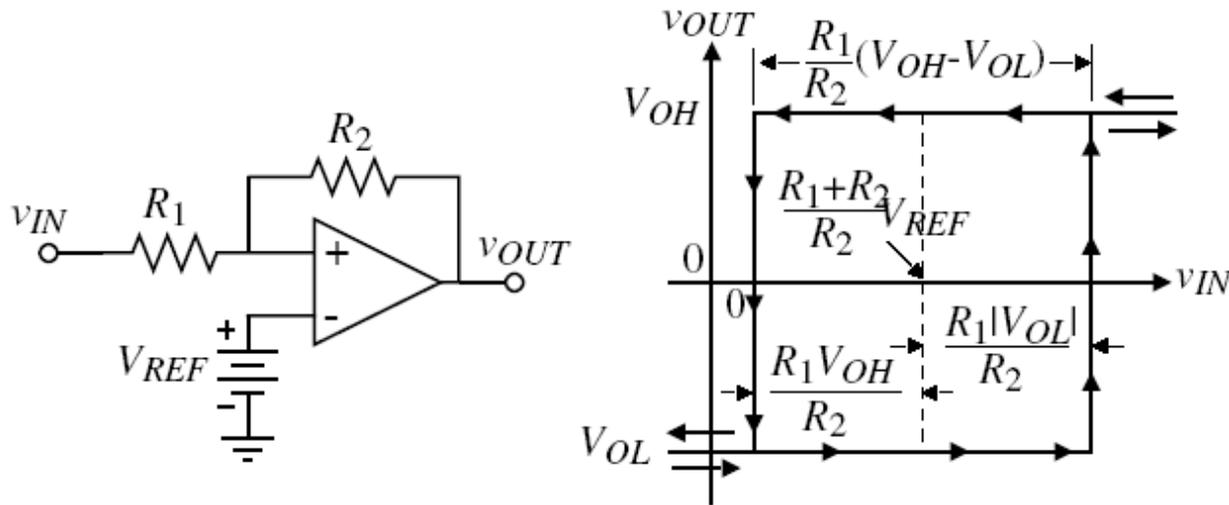
Hysteresis



Hysteresis

- The trip point is altered as a function of the input
- Can be achieved externally or internally

Hysteresis – External Feedback



Upper Trip Point

$$V_{REF} = \left(\frac{R_1}{R_1+R_2}\right)V_{OL} + \left(\frac{R_2}{R_1+R_2}\right)V_{TRP}^+$$

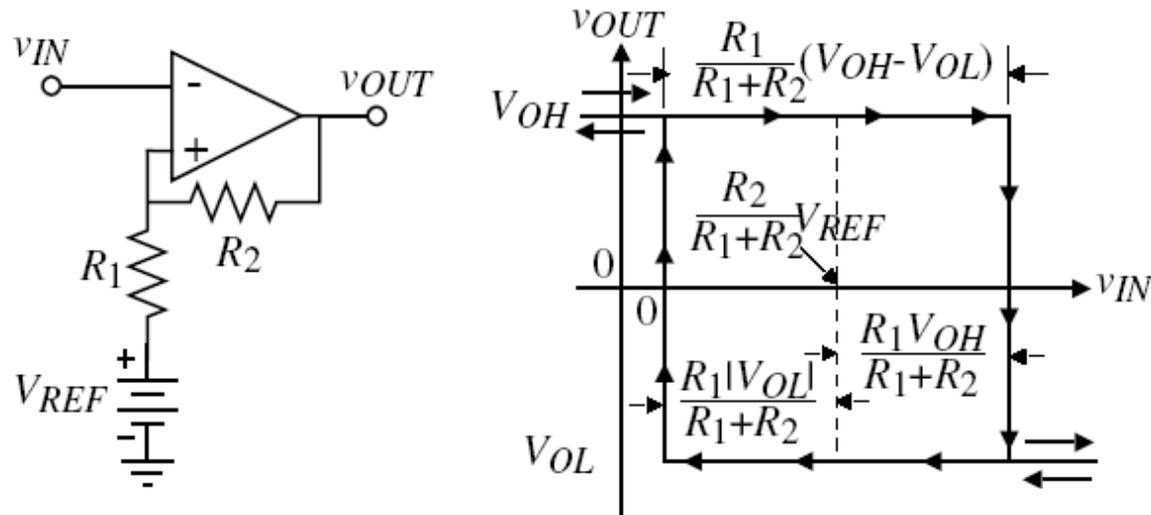
$$V_{TRP}^+ = \left(\frac{R_1+R_2}{R_2}\right)V_{REF} - \frac{R_1}{R_2}V_{OL}$$

Lower Trip Point

$$V_{REF} = \left(\frac{R_1}{R_1+R_2}\right)V_{OH} + \left(\frac{R_2}{R_1+R_2}\right)V_{TRP}^-$$

$$V_{TRP}^- = \left(\frac{R_1+R_2}{R_2}\right)V_{REF} - \frac{R_1}{R_2}V_{OH}$$

Hysteresis – External Feedback



Upper Trip Point

$$v_{IN} = V_{TRP}^+ = \left(\frac{R_1}{R_1 + R_2} \right) V_{OH} + \left(\frac{R_2}{R_1 + R_2} \right) V_{REF}$$

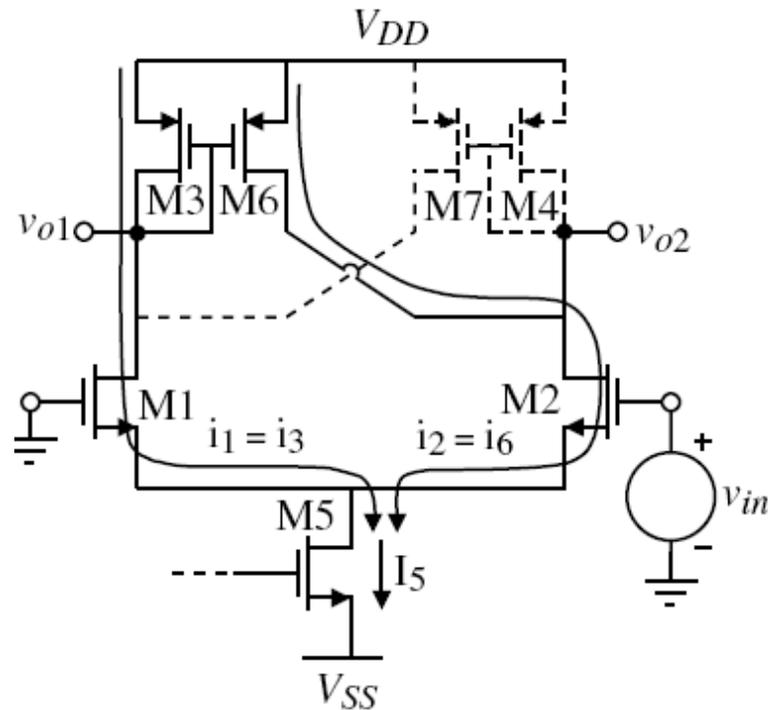
Lower Trip Point

$$v_{IN} = V_{TRP}^- = \left(\frac{R_1}{R_1 + R_2} \right) V_{OL} + \left(\frac{R_2}{R_1 + R_2} \right) V_{REF}$$

Hysteresis – Internal Feedback

Trip point occurs when current through M2 equals M6

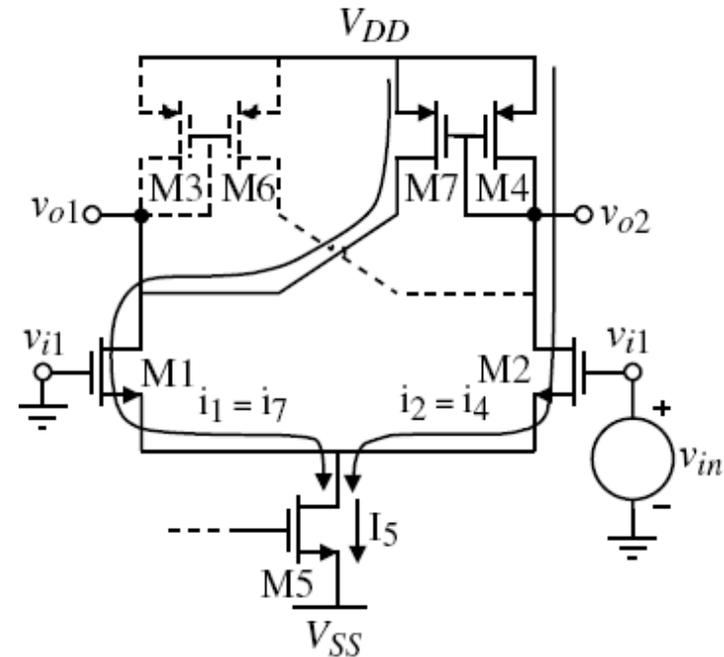
Any further increase will turn on M4/M7 setting the positive feedback in motion



Hysteresis – Internal Feedback

Trip point occurs when current through M1 equals M7

Any further increase will turn on M3/M6 setting the positive feedback in motion



Schmitt Trigger

Assume V_{in} low and V_{out} high

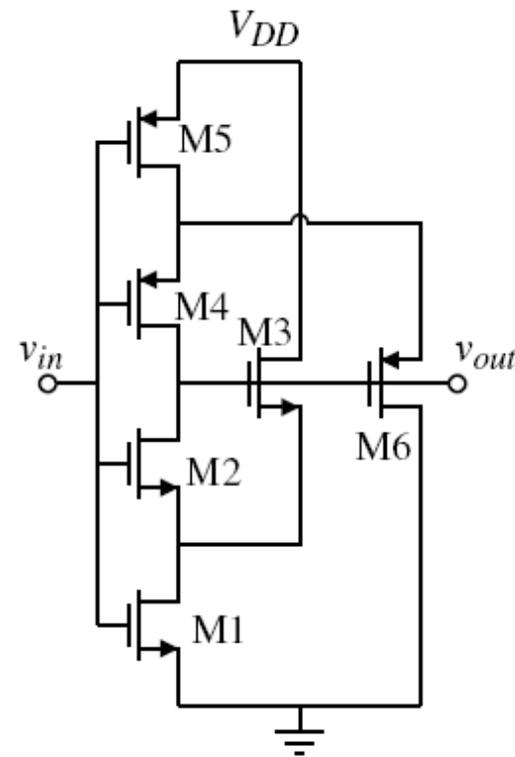
Transistors M1/M2/M6 are off

Transistors M3/M4/M5 are on

As V_{in} is increased M1 turns on

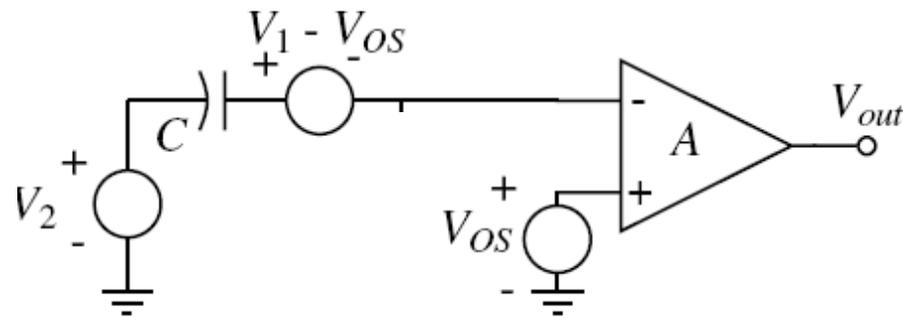
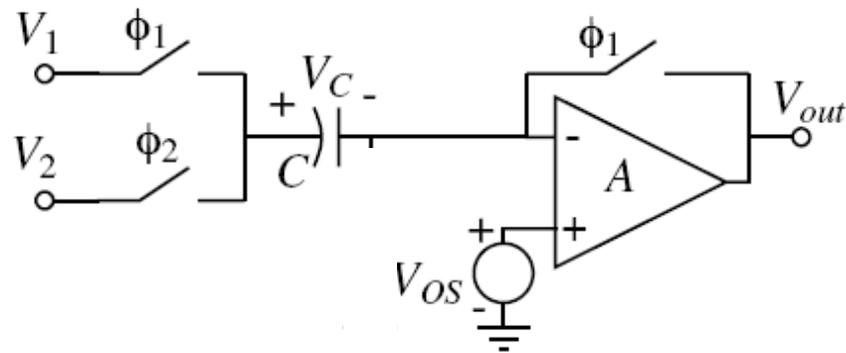
$I(M1)$ initially supplied by M3

When M2 turns on it decreases V_{out}
that turns off M3 and further
turns on M2 \rightarrow Positive feedback



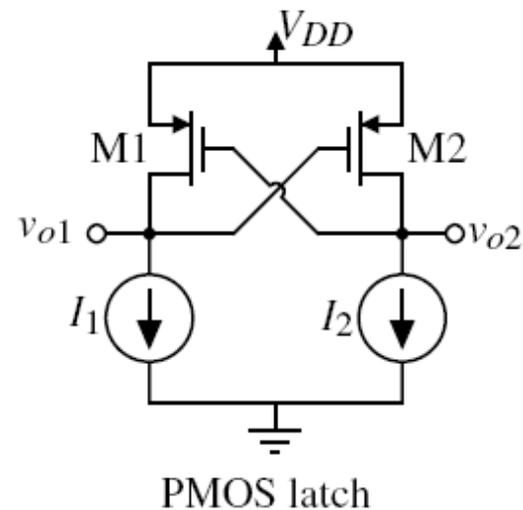
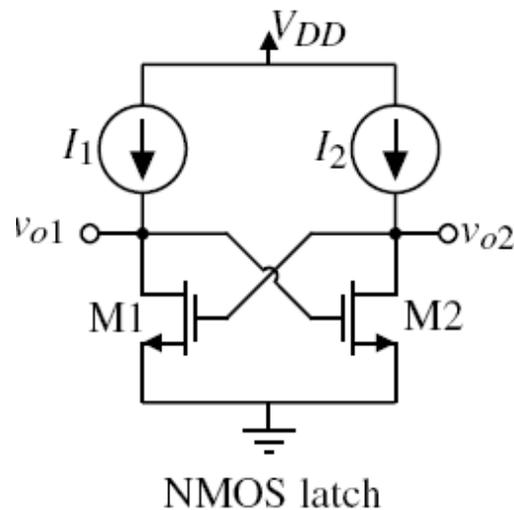
Trip point occurs at the point of turn on of M2

Switch Capacitor Comparator



ϕ_1 autozeroes the comparator and ϕ_2 performs the comparison

Regenerative Comparators



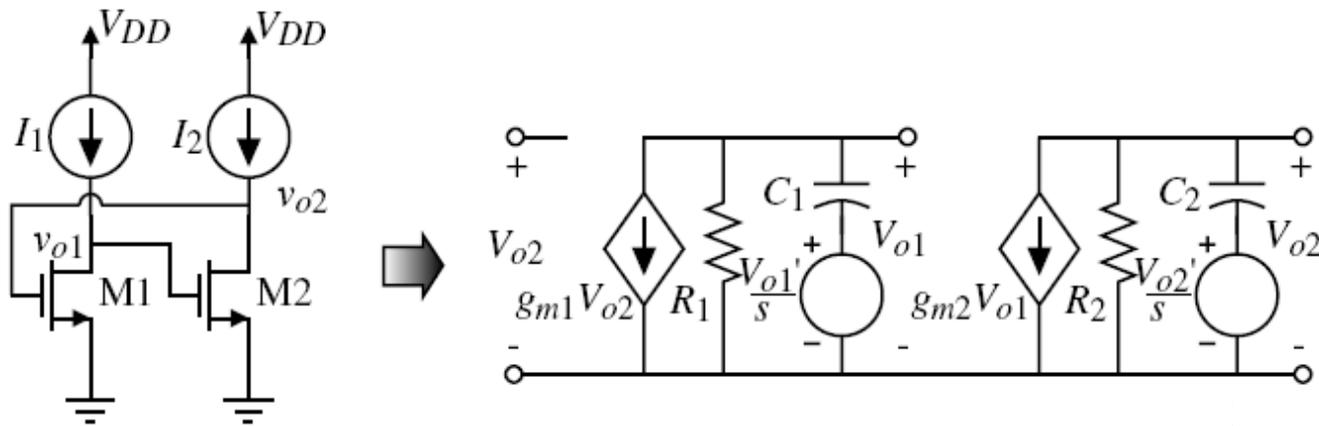
Use positive feedback to achieve signal comparison

The inputs are initially applied to the outputs of the latch.

V_{o1}' = initial input applied to v_{o1}

V_{o2}' = initial input applied to v_{o2}

Regenerative Comparators



$$g_{m1}V_{o2} + G_1V_{o1} + sC_1\left(V_{o1} - \frac{V_{o1}'}{s}\right) = g_{m1}V_{o2} + G_1V_{o1} + sC_1V_{o1} - C_1V_{o1}' = 0$$

$$g_{m2}V_{o1} + G_2V_{o2} + sC_2\left(V_{o2} - \frac{V_{o2}'}{s}\right) = g_{m2}V_{o1} + G_2V_{o2} + sC_2V_{o2} - C_2V_{o2}' = 0$$

Defining the output, ΔV_o , and input, ΔV_i , as

$$\Delta V_o = V_{o2} - V_{o1} \quad \text{and} \quad \Delta V_i = V_{o2}' - V_{o1}'$$

Regenerative Comparators

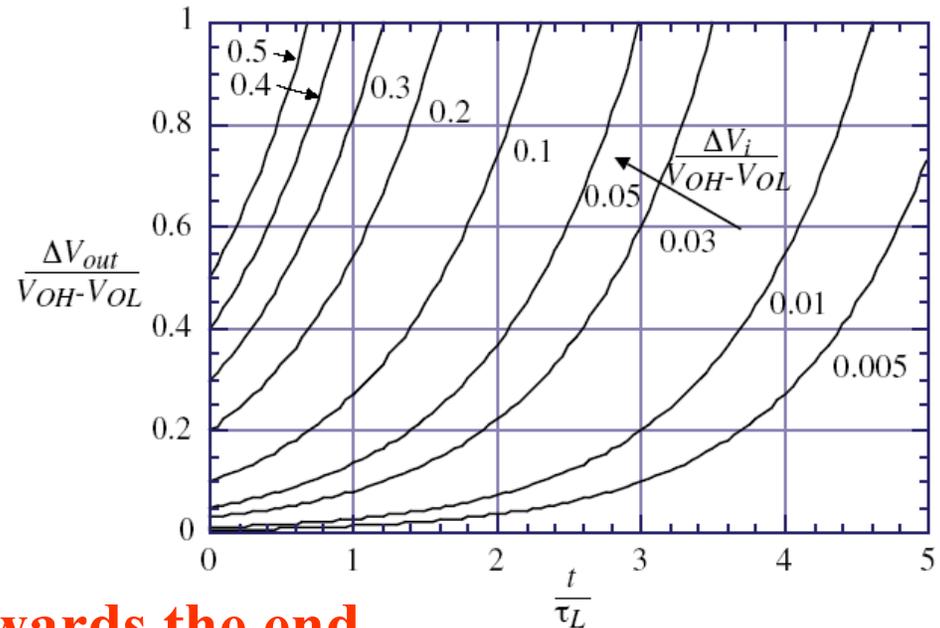
Solving

$$\Delta V_o = \frac{\tau \Delta V_i}{s\tau + (1 - g_m R)} = \frac{\frac{\tau \Delta V_i}{1 - g_m R}}{s\tau + 1} = \frac{\tau' \Delta V_i}{s\tau' + 1} \quad \tau' = \frac{\tau}{1 - g_m R}$$

Taking Inverse LT

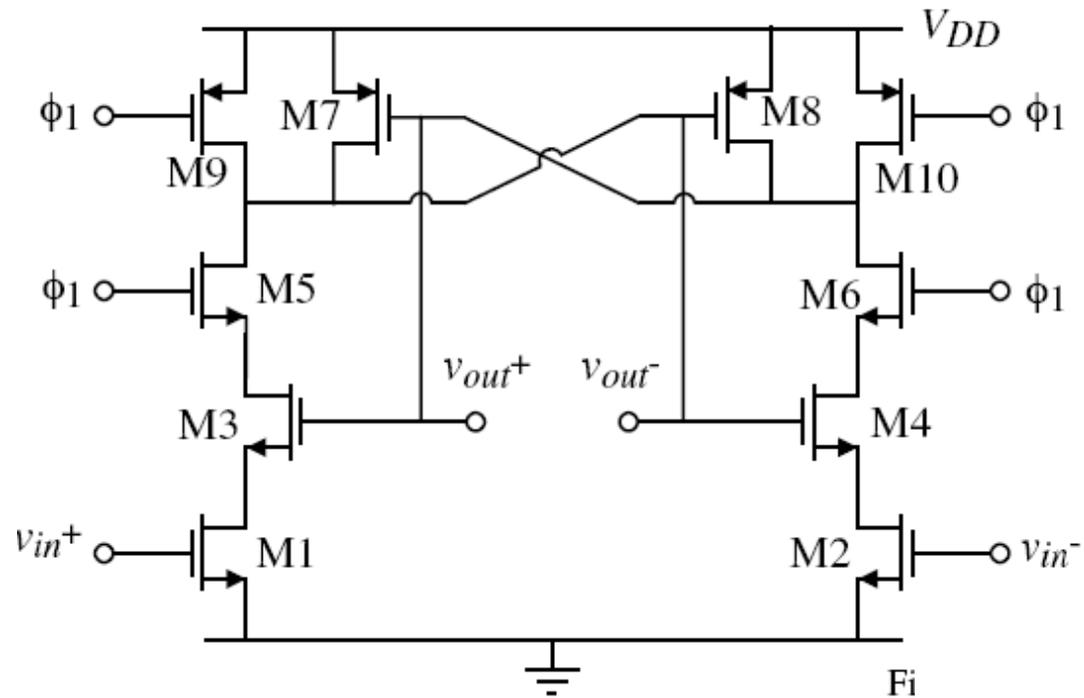
$$\Delta V_{out}(t) = e^{t/\tau_L} \Delta V_i$$

$$\tau_L = |\tau'| \approx \frac{\tau}{g_m R}$$



The response is rapid towards the end

Comparator using a Latch

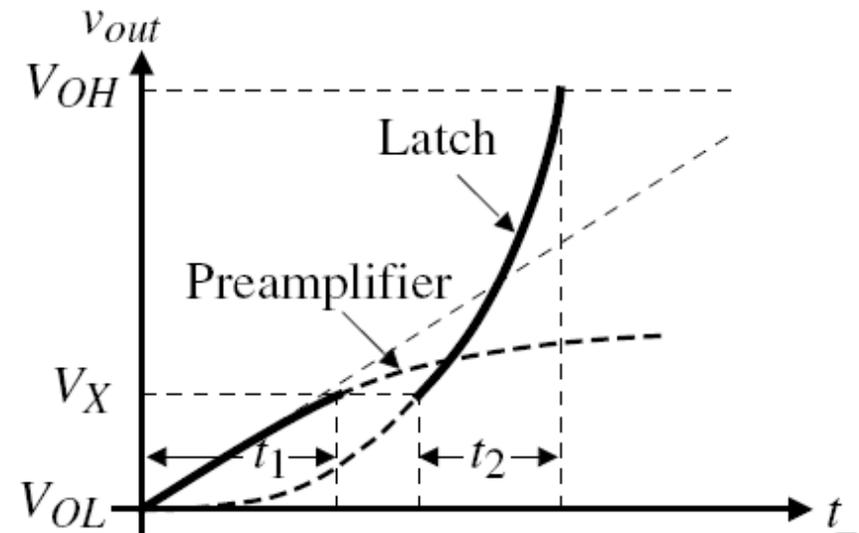


M1/M2 act as resistors degenerating M3/M4

High Speed Comparators

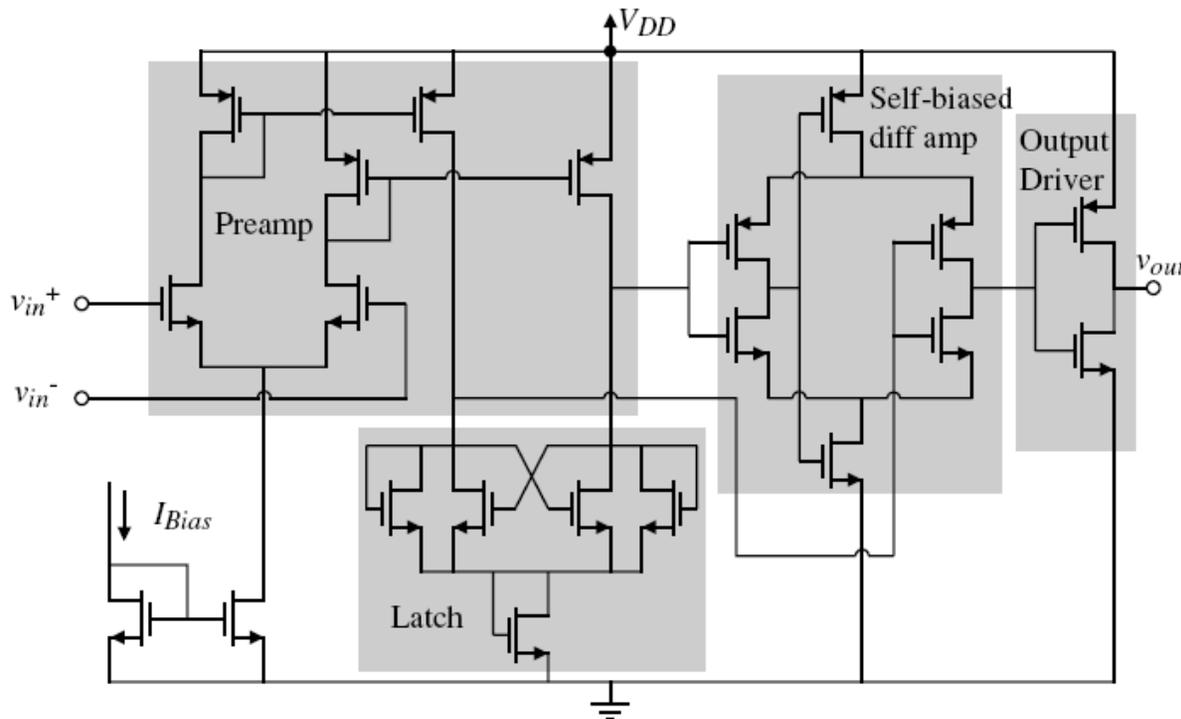
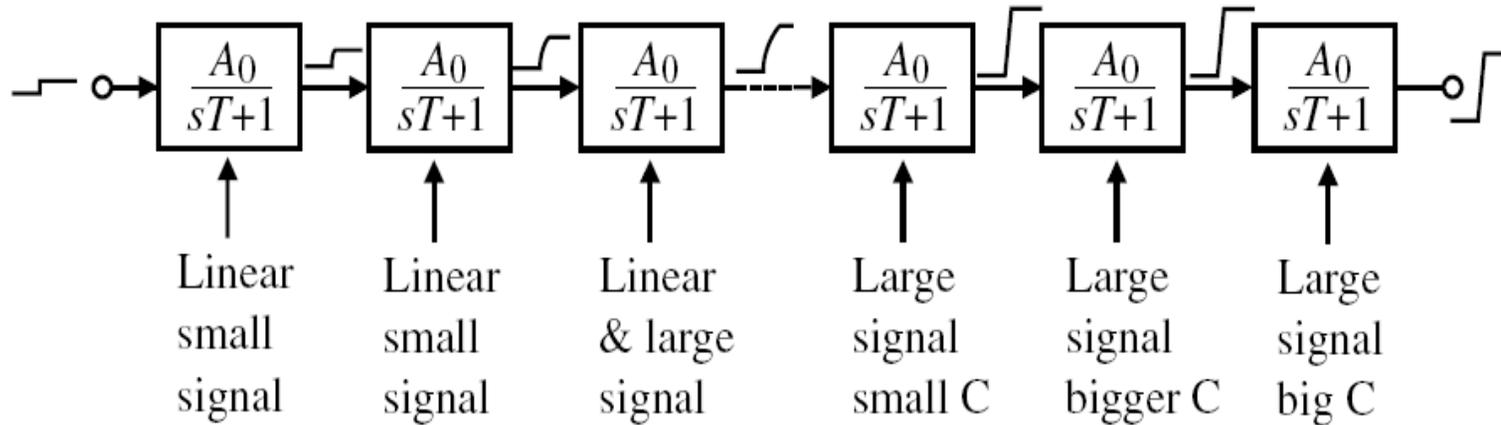
- Amplifiers have a step response with a negative argument in the exponent
- Latches have a step response with a positive argument in the exponent

Use a pre-amp to quickly build up the signal and pass it on to a latch!



Judicious use of both amplifier and latch to achieve high speeds

High Speed Comparators



Cascade of stages

Initial stages are responsible for signal buildup

Latter stages make a quick transition to binary levels

Summary

- Comparator Types
 - High Gain Open Loop Comparators
 - Improvements include autozeroing/hysteresis
 - Charge Injection Key Limitation
 - Discrete Time Comparators
 - Regenerative Comparators
 - High Speed Comparators
 - Pre-amp (High GB) + Latch + Output stage

Phillip E. Allen and Douglas R. Holberg, *CMOS Analog Circuit Design*. Oxford University Press, 2nd Edition, New York, 2003.